

MEMORANDUM

S-002-2021

TO: Michael Carpenter, P.E.
Director, Division of Structural Design

FROM: Geotechnical Branch
Division of Structural Design

BY: Tyler Sheffield, P.E.
Geotechnical Branch, Structure Foundations Section

DATE: October 25, 2021

SUBJECT: **Jefferson County**
Item No. 5-804.00
12F0 FD52 056 0264 021-023D;
MARS No. 8556402D
Fed. Num. 00STP2641176
RECONSTRUCT THE WATTERSON EXPRESSWAY INTERCHANGE
@US 42 INCLUDING SLIP RAMP TO KY 22
Single Span Bridge (~213') on I-264 EB over I-71 NB and I-71 SB Ramp to
I-264 WB
Geotechnical Engineering Structure Foundation Report

1.0 LOCATION AND DESCRIPTION

The geotechnical investigation for this structure has been completed. The DGN file for the subsurface data sheet has been made available on ProjectWise and through email for use in the development of structure plans. The drilling for this project was performed by the consulting firm of American Engineers Inc. (AEI).

The proposed bridge replacement is part of a project to reconstruct the I-264 interchange with US 42. The structure is located at approximate I-264 EB mile point 22.9. It spans I-71 NB and I-71 SB ramp to I-264. The project is located in Louisville, KY.

The existing bridge at this location is on top of a rock cut and founded on spread footings. The footings are in very close proximity to the rock cut face which exhibits weathering and rock pop-outs.

2.0 SITE GEOLOGIC CONDITIONS

This structure is located in the Jeffersonville, New Albany, and Charlestown Geologic Quadrangle (GQ# 1211). The geologic mapping indicates that the bedrock at this site consists of the Sellersburg Limestone and Lousiville Limestone Formations.

3.0 FIELD INVESTIGATION

Four (4) sample and core holes were taken for this structure. The drill crew delivered the rock core and soil samples to the KYTC Geotechnical Branch in Frankfort where a geologist logged the rock cores and the soil samples were classified and tested in the Branch's laboratory.

4.0 LABORATORY TESTING

The laboratory soil testing was completed by the Geotechnical Branch. The soil samples

obtained from the borings were determined to consist of inorganic high plasticity clays and clayey silty sands. The soil samples were designated CH, and SC-SM using the Unified Soil Classification System.

5.0 SUBSURFACE CONDITIONS

Depths to rock/refusal varied from 2.8 ft. to 21.0 ft. Rock cores from this location indicated that bedrock consists mostly of gray fine to medium grain, crystalline, dolomitic limestone with few stylolites. The KY RQD values for the rock cores taken at this proposed bridge location ranged from 74% to 100% and core recoveries ranged from 85% to 100%. The variation in top of rock/auger refusal elevations are in the table below. varied from 516.6 ft. to 565.6 ft.

Substructure Unit	Top of Rock Elevation (ft)
Abutment 1	535.9 to 565.6
Abutment 2	516.6 to 548.7

6.0 ENGINEERING ANALYSIS

ABUTMENT 1 & 2

6.1 Drilled Shafts

Use drilled shafts constructed in accordance with the Special Note for Drilled Shafts. The shaft tips shall extend a minimum of two shaft diameters below the bottom of permanent casing. Drilled shafts were evaluated for axial loading, and the attached tables provide the resulting capacities and resistances for LRFD methods. The elevations in the following table are needed to both complete the design and determine plan quantities for the drilled shafts. These elevations will be verified after construction phase drilling has been performed. The final shaft tip elevations and quantities may be adjusted based on actual field conditions. The highest tip elevation noted in the following table is based on a 3.5 ft. shaft diameter.

	Abutment 1	Abutment 2
Estimated Top of Rock	565.5	548.5
Estimated Bottom of Permanent Casing/Top of Rock Socket	565.5	548.5
Highest Allowable Shaft Tip	558.5	541.5

7.0 FOUNDATION RECOMMENDATIONS

7.1 Drilled Shafts (Abutment 1 & 2)

- 7.1.1 Use Drilled Shaft foundations with estimated top of rock socket elevations as noted in Sections 6.1 of this report.
- 7.1.2 The nearest edge of drilled shafts must be a minimum of 10 feet from the rock cut face.
- 7.1.3 Permanent casing is required in the overburden. It should be noted in the plans that the permanent casing is incidental to the unit bid price for

Drilled Shaft, Common or Solid Rock, as applicable. Use permanent casing that is 6 inches larger in diameter than the proposed shaft diameter to the “Bottom of Permanent Casing” elevations noted above. Casings shall meet the requirements of Section 2.3 of the Special Note for Drilled Shafts.

- 7.1.4 Permanent casing may need to be extended through any significant void, should they be encountered. Shaft tip elevations may also need to be lowered if significant voids are encountered.
- 7.1.5 Require a 6-inch minimum rebar cover in the uncased rock sockets.
- 7.1.6 For Load & Resistance Factor Design (LRFD), evaluate the total factored axial resistances using the attached Drilled Shaft Axial Resistance Tables considering the capacity developed in the uncased rock sockets. The total factored resistances must exceed the factored loads at the strength limit state. The highest allowable tip elevations are provided in Sections 6.1 of this report. Longer uncased sockets may be required to satisfy axial or lateral load design criteria.
- 7.1.7 Perform lateral load analysis using the geotechnical parameters provided in the attached Idealized Soil and Bedrock Profiles. These parameters may be used to perform analyses using LPILE or other similar software. Some of the parameters may not be required to input, depending on the version of software utilized. Design the substructure units neglecting any lateral resistance from the overburden.
- 7.1.8 Additional drilling will be required at each drilled shaft location as noted in Section 3.5, Subsurface Investigation of the Special Note for Drilled Shafts. Estimates of the amount of Rockline Sounding may be made by taking the difference between the ground surface and the rockline at each shaft location. For estimating the amount of Rock Coring at this location, we recommend that the subsurface exploration extend a minimum depth of three (3) shaft diameters (but not less than 10 feet) below the bottom of the anticipated tip elevation of each drilled shaft.
- 7.1.9 Use the elevations in Sections 6.1 of this report to determine plan quantities as follows:
 - Drilled Shaft - *-inch (Common) - Top of shaft to Top of Rock
 - Drilled Shaft - **-inch (Solid Rock) - Bottom of Permanent Casing to Shaft Tip
 - * - Insert diameter 6-inches larger than shaft diameter chosen
 - ** - Shaft diameter (Rock Socket diameter) chosen
 - The final shaft tip elevations and quantities may be adjusted based on the actual conditions encountered in the field.

8.0 PLAN NOTES

(Include the notes below at appropriate locations in the plans, if applicable.)

- 8.1 Temporary sheeting and/or shoring may be required for installation of drilled

- shafts.
- 8.2** Permanent casing is required in the overburden. Permanent casing will also be required through portions of solid rock where voids or karst features may be found. Permanent casing is incidental to the unit bid price for "Drilled Shaft - ____-inch (Common)" or "Drilled Shaft - ____-inch (Solid Rock) as applicable. (Insert shaft sizes 6" larger than the chosen drilled shaft rock socket diameter as noted in Section 7.1.9 of this report.)
- 8.3** Drilled shafts shall be constructed in accordance with the Special Note for Drilled Shafts. Include all costs (labor, equipment, and materials including spiral and longitudinal reinforcement, reinforcement splices, mechanical couplers, concrete, and temporary or permanent casing) associated with the drilled shafts in the unit price bid for Drilled Shaft, Common or Solid Rock, as applicable.
- 8.4** The Contractor will be responsible for providing subsurface exploration drilling during construction to finalize the drilled shaft tip elevations. Additional drilling will be required at each drilled shaft location in accordance with the Special Note for Drilled Shafts, current edition.

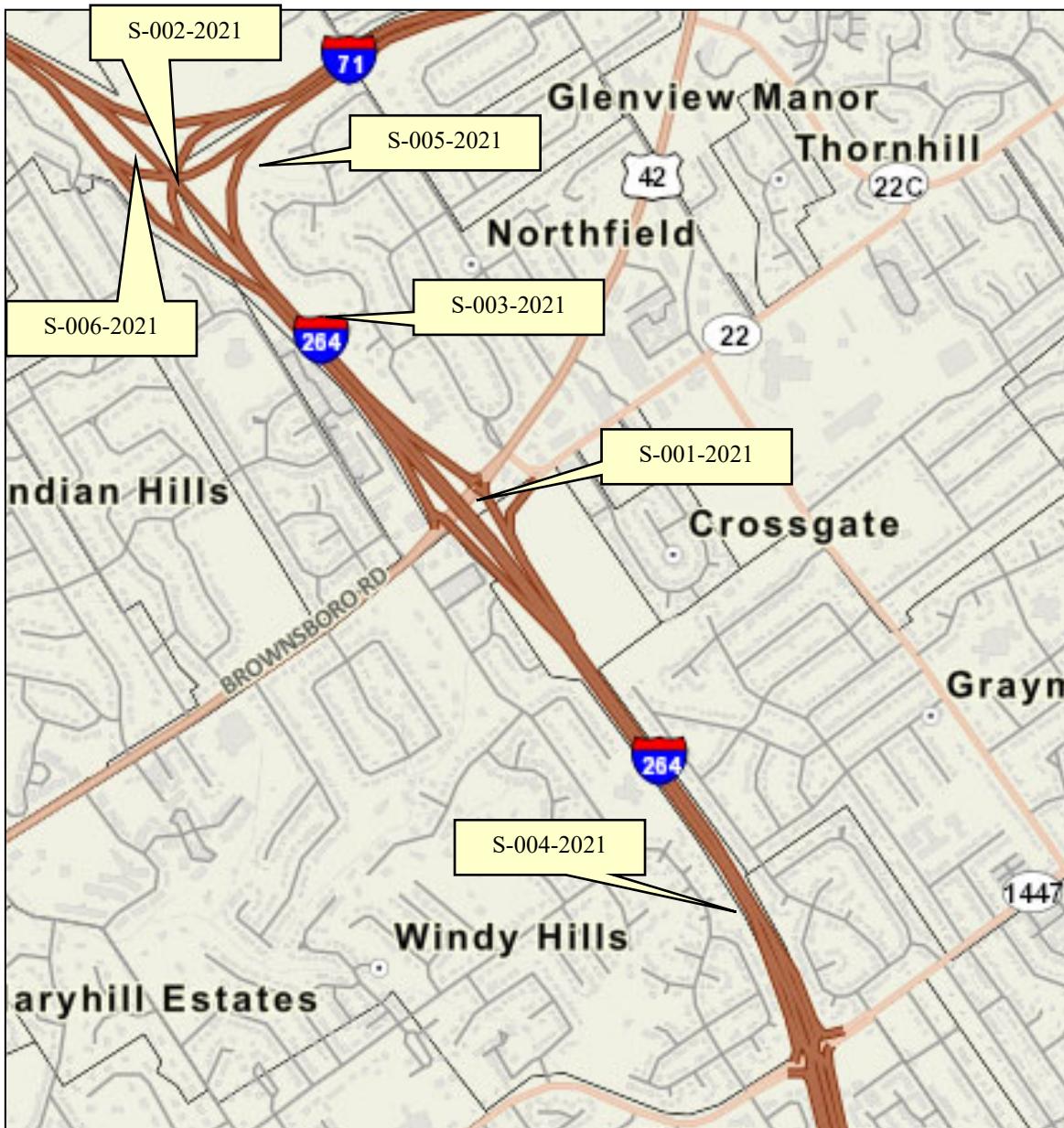
The designer should feel free to contact the Geotechnical Branch at 502-564-2374 for further recommendations or if any questions arise pertaining to this project.

Attachments:

- **Project Location Map**
- **Subsurface Data Sheet**
- **Idealized Soil and Bedrock Profile**
- **Drilled Shaft Axial Resistance Table**
- **Coordinate Data Sheet**

S-002-2021
Jefferson Co., I-264
October 25, 2021
Item #: 5-804.00

Project Location Map



SUBSURFACE DATA

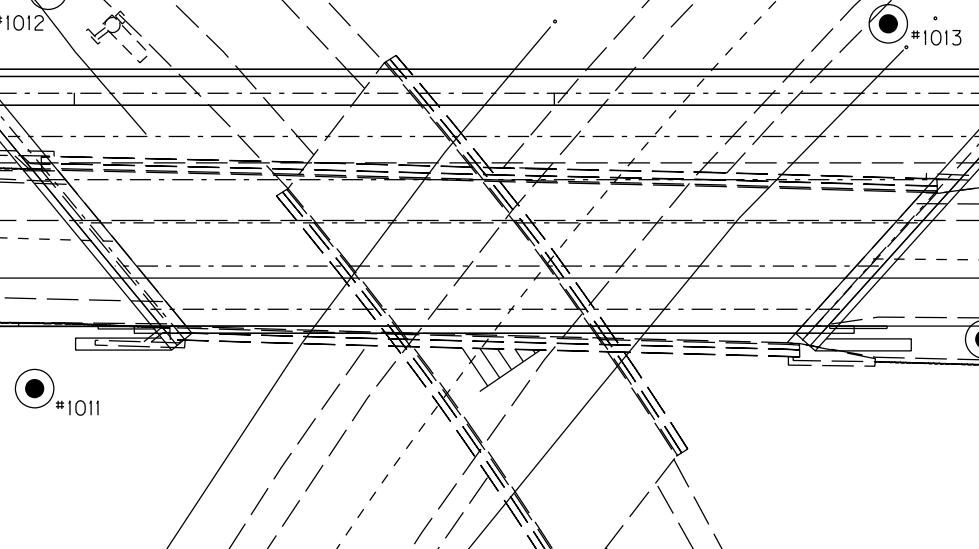
Plan Scale 1" = 20'

45+00

47+00

48+00

49+00



Profile Scale:
Vertical 1" = 10'
Horizontal not to scale

END BENT ONE

APPROXIMATE ROADWAY GRADE ELEV. = 571.36

Hole No.
Station
Offset
Elev.
(NAVD 88
datum)

1011
45+91.70
59.00 ft. Rt.
570.50

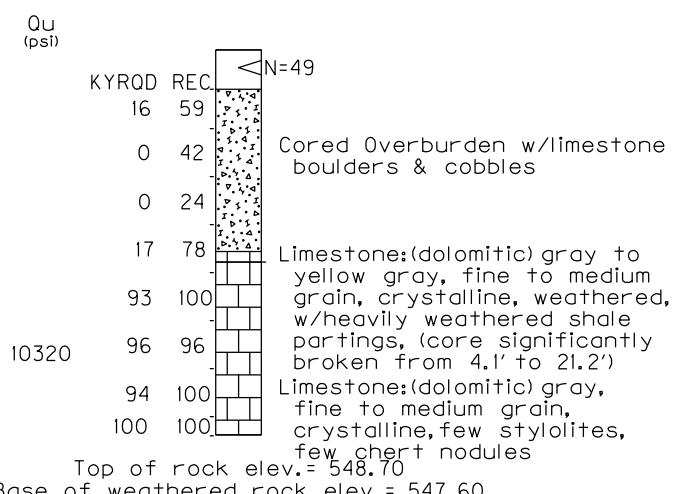
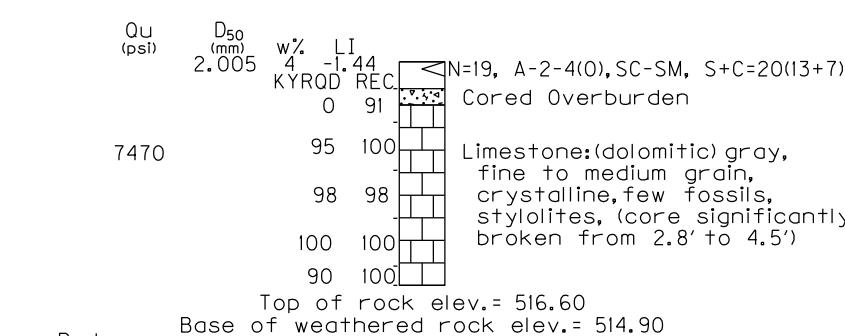
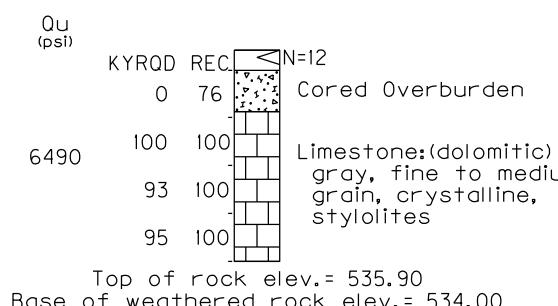
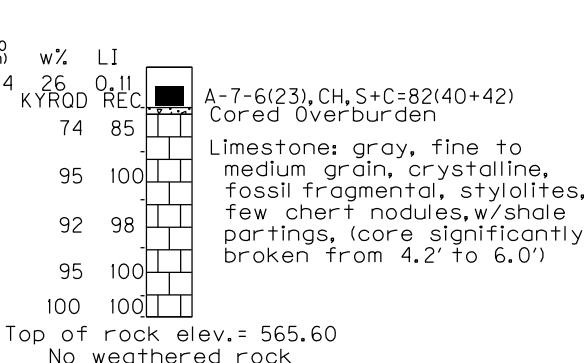
1012
45+94.50
24.00 ft. Lt.
540.40

1013
47+69.60
17.00 ft. Lt.
519.40

1014
47+89.70
48.80 ft. Rt.
569.70

END BENT TWO

APPROXIMATE ROADWAY GRADE ELEV. = 569.78



COMMONWEALTH OF KENTUCKY
DEPARTMENT OF HIGHWAYS



REVISION

DATE

PREPARED BY
Division of Structural Design
Geotechnical Branch

DATE: 18-OCTOBER-2021

CHECKED BY

DESIGNED BY:

DETAILED BY: E. BAILEY

T. SHEFFIELD

CROSSING
I-264 Bridge over I-71 Ramp

ROUTE
I-264

ITEM NO.
5-804.00

COUNTY OF
JEFFERSON

SHEET NO.

DRAWING NUMBER
S-002-2021

IDEALIZED SOIL AND BEDROCK PROFILE

S-002-2021: Jefferson Co., Item# 5-804.00, I-264 over I-71

TQS 10/14/2021



Overburden, Neglect for Support
Stiff Clay w/ Free Water

Effective Unit Weight,	γ_e (lb/ft ³) =	120
Undrained Cohesion,	c (lb/ft ²) =	2500
Strain Factor,	E50 =	0.005
Soil Modulus,	k (lb/in ³) =	1000

Top of Rock Socket

*

Strata Parameters for Lateral Load Analyses

Limestone

Strong Rock (Vuggy Limestone)

γ_t (lb/ft ³) =	150	Effective Unit Weight,	γ_e (lb/in ³) =	0.087
q _u (psi) =	4800	Unaxial Compressive Strength,	q _u (psi) =	4800
q _{eb} (ksf) =	72			
f _s (ksf) =	32.7			

(Side friction limited by Concrete Strength to f_s = 32.7 ksf)

*

Shaft Tip

- * Elevations vary and are provided in the report body.

ADDITIONAL DATA FOR GEOTECHNICAL CALCULATIONS ONLY:

min. f _c (psi) =	3500
p _a (psi) =	14.7

Load and Resistance Factor Design (LRFD)

DRILLED SHAFT AXIAL RESISTANCE TABLE

S-002-2021: Jefferson Co., Item# 5-804.00, I-264 over I-71

Rock Socket Diameter = 3.5 feet
 Rock Socket Diameter = 42 inches TQS 10/14/2021

Rock Socket Length (ft.)	Nominal Unit Side Shear q_{ss} (ksf)	Nominal Unit End Bearing q_{eb} (ksf)	Nominal Side Resistance R_{sr} (kips)	Nominal End Bearing Resistance R_{eb} (kips)	Factored Side Resistance ϕR_{sr} (kips)	Factored End Bearing Resistance ϕR_{eb} (kips)	Total Factored Axial Resistance ϕR_t (kips)	Total Factored Uplift Resistance ϕR_{tu} (kips)
0.0								
1.0	32.7	72	359	693	198	346	544	144
2.0	32.7	72	718	693	395	346	741	287
3.0	32.7	72	1077	693	593	346	939	431
4.0	32.7	72	1437	693	790	346	1136	575
5.0	32.7	72	1796	693	988	346	1334	718
6.0	32.7	72	2155	693	1185	346	1532	862
>>>	7.0	32.7	2514	693	1383	346	1729	1006
	8.0	32.7	2873	693	1580	346	1927	1149
	9.0	32.7	3232	693	1778	346	2124	1293
	10.0	32.7	3591	693	1975	346	2322	1437
	11.0	32.7	3951	693	2173	346	2519	1580
	12.0	32.7	4310	693	2370	346	2717	1724
	13.0	32.7	4669	693	2568	346	2914	1868
	14.0	32.7	5028	693	2765	346	3112	2011
	15.0	32.7	5387	693	2963	346	3309	2155
	16.0	32.7	5746	693	3160	346	3507	2299
	17.0	32.7	6106	693	3358	346	3704	2442
	18.0	32.7	6465	693	3556	346	3902	2586
	19.0	32.7	6824	693	3753	346	4099	2730
	20.0	32.7	7183	693	3951	346	4297	2873
AASHTO Table 10.5.5.2.4-1				Resistance Factor, ϕ	0.55	0.50		0.40
AASHTO 10.5.5.2.4: *When applying this table to a single shaft supporting a bridge pier, reduce the factored resistance by another 20%.								
>>> = Min. Socket Length							D (ft.) =	3.5

Load and Resistance Factor Design (LRFD)

DRILLED SHAFT AXIAL RESISTANCE TABLE

S-002-2021: Jefferson Co., Item# 5-804.00, I-264 over I-71

Rock Socket Diameter = 4.0 feet
 Rock Socket Diameter = 48 inches TQS 10/14/2021

Rock Socket Length (ft.)	Nominal Unit Side Shear q_{ss} (ksf)	Nominal Unit End Bearing q_{eb} (ksf)	Nominal Side Resistance R_{sr} (kips)	Nominal End Bearing Resistance R_{eb} (kips)	Factored Side Resistance ϕR_{sr} (kips)	Factored End Bearing Resistance ϕR_{eb} (kips)	Total Factored Axial Resistance ϕR_t (kips)	Total Factored Uplift Resistance ϕR_{tu} (kips)
0.0								
1.0	32.7	72	410	905	226	452	678	164
2.0	32.7	72	821	905	451	452	904	328
3.0	32.7	72	1231	905	677	452	1130	493
4.0	32.7	72	1642	905	903	452	1355	657
5.0	32.7	72	2052	905	1129	452	1581	821
6.0	32.7	72	2463	905	1354	452	1807	985
7.0	32.7	72	2873	905	1580	452	2033	1149
>>>	8.0	32.7	72	3284	905	1806	452	2258
	9.0	32.7	72	3694	905	2032	452	2484
	10.0	32.7	72	4105	905	2257	452	2710
	11.0	32.7	72	4515	905	2483	452	2936
	12.0	32.7	72	4925	905	2709	452	3161
	13.0	32.7	72	5336	905	2935	452	3387
	14.0	32.7	72	5746	905	3160	452	3613
	15.0	32.7	72	6157	905	3386	452	3839
	16.0	32.7	72	6567	905	3612	452	4064
	17.0	32.7	72	6978	905	3838	452	4290
	18.0	32.7	72	7388	905	4063	452	4516
	19.0	32.7	72	7799	905	4289	452	4742
	20.0	32.7	72	8209	905	4515	452	4967
AASHTO Table 10.5.5.2.4-1				Resistance Factor, ϕ	0.55	0.50		0.40
AASHTO 10.5.5.2.4: *When applying this table to a single shaft supporting a bridge pier, reduce the factored resistance by another 20%.								
>>> = Min. Socket Length							D (ft.) =	4.0

Load and Resistance Factor Design (LRFD)

DRILLED SHAFT AXIAL RESISTANCE TABLE

S-002-2021: Jefferson Co., Item# 5-804.00, I-264 over I-71

Rock Socket Diameter = 4.5 feet
 Rock Socket Diameter = 54 inches TQS 10/14/2021

Rock Socket Length (ft.)	Nominal Unit Side Shear q_{ss} (ksf)	Nominal Unit End Bearing q_{eb} (ksf)	Nominal Side Resistance R_{sr} (kips)	Nominal End Bearing Resistance R_{eb} (kips)	Factored Side Resistance ϕR_{sr} (kips)	Factored End Bearing Resistance ϕR_{eb} (kips)	Total Factored Axial Resistance ϕR_t (kips)	Total Factored Uplift Resistance ϕR_{tu} (kips)
0.0								
1.0	32.7	72	462	1145	254	573	827	185
2.0	32.7	72	924	1145	508	573	1080	369
3.0	32.7	72	1385	1145	762	573	1334	554
4.0	32.7	72	1847	1145	1016	573	1588	739
5.0	32.7	72	2309	1145	1270	573	1842	924
6.0	32.7	72	2771	1145	1524	573	2096	1108
7.0	32.7	72	3232	1145	1778	573	2350	1293
8.0	32.7	72	3694	1145	2032	573	2604	1478
>>> 9.0	32.7	72	4156	1145	2286	573	2858	1662
10.0	32.7	72	4618	1145	2540	573	3112	1847
11.0	32.7	72	5079	1145	2794	573	3366	2032
12.0	32.7	72	5541	1145	3048	573	3620	2216
13.0	32.7	72	6003	1145	3302	573	3874	2401
14.0	32.7	72	6465	1145	3556	573	4128	2586
15.0	32.7	72	6926	1145	3810	573	4382	2771
16.0	32.7	72	7388	1145	4063	573	4636	2955
17.0	32.7	72	7850	1145	4317	573	4890	3140
18.0	32.7	72	8312	1145	4571	573	5144	3325
19.0	32.7	72	8773	1145	4825	573	5398	3509
20.0	32.7	72	9235	1145	5079	573	5652	3694
AASHTO Table 10.5.5.2.4-1				Resistance Factor, ϕ	0.55	0.50		0.40
AASHTO 10.5.5.2.4: *When applying this table to a single shaft supporting a bridge pier, reduce the factored resistance by another 20%.								
>>> = Min. Socket Length							D (ft.) =	4.5

Load and Resistance Factor Design (LRFD)

DRILLED SHAFT AXIAL RESISTANCE TABLE

S-002-2021: Jefferson Co., Item# 5-804.00, I-264 over I-71

Rock Socket Diameter = 5.0 feet
 Rock Socket Diameter = 60 inches

TQS 10/14/2021

Rock Socket Length (ft.)	Nominal Unit Side Shear q_{ss} (ksf)	Nominal Unit End Bearing q_{eb} (ksf)	Nominal Side Resistance R_{sr} (kips)	Nominal End Bearing Resistance R_{eb} (kips)	Factored Side Resistance ϕR_{sr} (kips)	Factored End Bearing Resistance ϕR_{eb} (kips)	Total Factored Axial Resistance ϕR_t (kips)	Total Factored Uplift Resistance ϕR_{tu} (kips)
0.0								
1.0	32.7	72	513	1414	282	707	989	205
2.0	32.7	72	1026	1414	564	707	1271	410
3.0	32.7	72	1539	1414	847	707	1553	616
4.0	32.7	72	2052	1414	1129	707	1836	821
5.0	32.7	72	2565	1414	1411	707	2118	1026
6.0	32.7	72	3078	1414	1693	707	2400	1231
7.0	32.7	72	3591	1414	1975	707	2682	1437
8.0	32.7	72	4105	1414	2257	707	2964	1642
9.0	32.7	72	4618	1414	2540	707	3247	1847
>>>	10.0	32.7	5131	1414	2822	707	3529	2052
	11.0	32.7	5644	1414	3104	707	3811	2257
	12.0	32.7	6157	1414	3386	707	4093	2463
	13.0	32.7	6670	1414	3668	707	4375	2668
	14.0	32.7	7183	1414	3951	707	4657	2873
	15.0	32.7	7696	1414	4233	707	4940	3078
	16.0	32.7	8209	1414	4515	707	5222	3284
	17.0	32.7	8722	1414	4797	707	5504	3489
	18.0	32.7	9235	1414	5079	707	5786	3694
	19.0	32.7	9748	1414	5362	707	6068	3899
	20.0	32.7	10261	1414	5644	707	6351	4105
AASHTO Table 10.5.5.2.4-1				Resistance Factor, ϕ	0.55	0.50		0.40
AASHTO 10.5.5.2.4: *When applying this table to a single shaft supporting a bridge pier, reduce the factored resistance by another 20%.								
>>> = Min. Socket Length							D (ft.) =	5.0

Load and Resistance Factor Design (LRFD)

DRILLED SHAFT AXIAL RESISTANCE TABLE

S-002-2021: Jefferson Co., Item# 5-804.00, I-264 over I-71

Rock Socket Length (ft.)	Rock Socket Diameter =		5.5 feet		Factored End Bearing Resistance		Total Factored Axial Resistance	Total Factored Uplift Resistance
	Nominal Unit Side Shear q_{ss} (ksf)	Nominal Unit End Bearing q_{eb} (ksf)	Nominal Side Resistance R_{sr} (kips)	Nominal End Bearing Resistance R_{eb} (kips)	Factored Side Resistance ϕR_{sr} (kips)	Factored End Bearing Resistance ϕR_{eb} (kips)		
0.0								
1.0	32.7	72	564	1711	310	855	1166	226
2.0	32.7	72	1129	1711	621	855	1476	451
3.0	32.7	72	1693	1711	931	855	1787	677
4.0	32.7	72	2257	1711	1242	855	2097	903
5.0	32.7	72	2822	1711	1552	855	2407	1129
6.0	32.7	72	3386	1711	1862	855	2718	1354
7.0	32.7	72	3951	1711	2173	855	3028	1580
8.0	32.7	72	4515	1711	2483	855	3339	1806
9.0	32.7	72	5079	1711	2794	855	3649	2032
10.0	32.7	72	5644	1711	3104	855	3959	2257
>>> 11.0	32.7	72	6208	1711	3414	855	4270	2483
12.0	32.7	72	6772	1711	3725	855	4580	2709
13.0	32.7	72	7337	1711	4035	855	4891	2935
14.0	32.7	72	7901	1711	4346	855	5201	3160
15.0	32.7	72	8466	1711	4656	855	5511	3386
16.0	32.7	72	9030	1711	4966	855	5822	3612
17.0	32.7	72	9594	1711	5277	855	6132	3838
18.0	32.7	72	10159	1711	5587	855	6443	4063
19.0	32.7	72	10723	1711	5898	855	6753	4289
20.0	32.7	72	11287	1711	6208	855	7063	4515
AASHTO Table 10.5.5.2.4-1			Resistance Factor, ϕ	0.55	0.50			0.40
AASHTO 10.5.5.2.4: *When applying this table to a single shaft supporting a bridge pier, reduce the factored resistance by another 20%.								
>>> = Min. Socket Length							D (ft.) =	5.5

Load and Resistance Factor Design (LRFD)

DRILLED SHAFT AXIAL RESISTANCE TABLE

S-002-2021: Jefferson Co., Item# 5-804.00, I-264 over I-71

Load and Resistance Factor Design (LRFD)

DRILLED SHAFT AXIAL RESISTANCE TABLE

S-002-2021: Jefferson Co., Item# 5-804.00, I-264 over I-71

Rock Socket Diameter = 6.5 feet
 Rock Socket Diameter = 78 inches TQS 10/14/2021

Rock Socket Length (ft.)	Nominal Unit Side Shear q_{ss} (ksf)	Nominal Unit End Bearing q_{eb} (ksf)	Nominal Side Resistance R_{sr} (kips)	Nominal End Bearing Resistance R_{eb} (kips)	Factored Side Resistance ϕR_{sr} (kips)	Factored End Bearing Resistance ϕR_{eb} (kips)	Total Factored Axial Resistance ϕR_t (kips)	Total Factored Uplift Resistance ϕR_{tu} (kips)
0.0								
1.0	32.7	72	667	2389	367	1195	1561	267
2.0	32.7	72	1334	2389	734	1195	1928	534
3.0	32.7	72	2001	2389	1101	1195	2295	800
4.0	32.7	72	2668	2389	1467	1195	2662	1067
5.0	32.7	72	3335	2389	1834	1195	3029	1334
6.0	32.7	72	4002	2389	2201	1195	3396	1601
7.0	32.7	72	4669	2389	2568	1195	3762	1868
8.0	32.7	72	5336	2389	2935	1195	4129	2134
9.0	32.7	72	6003	2389	3302	1195	4496	2401
10.0	32.7	72	6670	2389	3668	1195	4863	2668
11.0	32.7	72	7337	2389	4035	1195	5230	2935
12.0	32.7	72	8004	2389	4402	1195	5597	3202
>>>	13.0	32.7	72	8671	2389	4769	1195	5964
	14.0	32.7	72	9338	2389	5136	1195	6330
	15.0	32.7	72	10005	2389	5503	1195	6697
	16.0	32.7	72	10672	2389	5869	1195	7064
	17.0	32.7	72	11339	2389	6236	1195	7431
	18.0	32.7	72	12006	2389	6603	1195	7798
	19.0	32.7	72	12673	2389	6970	1195	8165
	20.0	32.7	72	13340	2389	7337	1195	8531
AASHTO Table 10.5.5.2.4-1				Resistance Factor, ϕ	0.55	0.50		0.40
AASHTO 10.5.5.2.4: *When applying this table to a single shaft supporting a bridge pier, reduce the factored resistance by another 20%.								
>>> = Min. Socket Length							D (ft.) =	6.5

Load and Resistance Factor Design (LRFD)

DRILLED SHAFT AXIAL RESISTANCE TABLE

S-002-2021: Jefferson Co., Item# 5-804.00, I-264 over I-71

Rock Socket Diameter = 7.0 feet
 Rock Socket Diameter = 84 inches TQS 10/14/2021

Rock Socket Length (ft.)	Nominal Unit Side Shear q_{ss} (ksf)	Nominal Unit End Bearing q_{eb} (ksf)	Nominal Side Resistance R_{sr} (kips)	Nominal End Bearing Resistance R_{eb} (kips)	Factored Side Resistance ϕR_{sr} (kips)	Factored End Bearing Resistance ϕR_{eb} (kips)	Total Factored Axial Resistance ϕR_t (kips)	Total Factored Uplift Resistance ϕR_{tu} (kips)
0.0								
1.0	32.7	72	718	2771	395	1385	1781	287
2.0	32.7	72	1437	2771	790	1385	2176	575
3.0	32.7	72	2155	2771	1185	1385	2571	862
4.0	32.7	72	2873	2771	1580	1385	2966	1149
5.0	32.7	72	3591	2771	1975	1385	3361	1437
6.0	32.7	72	4310	2771	2370	1385	3756	1724
7.0	32.7	72	5028	2771	2765	1385	4151	2011
8.0	32.7	72	5746	2771	3160	1385	4546	2299
9.0	32.7	72	6465	2771	3556	1385	4941	2586
10.0	32.7	72	7183	2771	3951	1385	5336	2873
11.0	32.7	72	7901	2771	4346	1385	5731	3160
12.0	32.7	72	8620	2771	4741	1385	6126	3448
13.0	32.7	72	9338	2771	5136	1385	6521	3735
>>>	14.0	32.7	10056	2771	5531	1385	6916	4022
	15.0	32.7	10774	2771	5926	1385	7311	4310
	16.0	32.7	11493	2771	6321	1385	7706	4597
	17.0	32.7	12211	2771	6716	1385	8102	4884
	18.0	32.7	12929	2771	7111	1385	8497	5172
	19.0	32.7	13648	2771	7506	1385	8892	5459
	20.0	32.7	14366	2771	7901	1385	9287	5746
AASHTO Table 10.5.5.2.4-1				Resistance Factor, ϕ	0.55	0.50		0.40
AASHTO 10.5.5.2.4: *When applying this table to a single shaft supporting a bridge pier, reduce the factored resistance by another 20%.								
>>> = Min. Socket Length							D (ft.) =	7.0

Load and Resistance Factor Design (LRFD)

DRILLED SHAFT AXIAL RESISTANCE TABLE

S-002-2021: Jefferson Co., Item# 5-804.00, I-264 over I-71

Rock Socket Diameter = 7.5 feet
 Rock Socket Diameter = 90 inches TQS 10/14/2021

Rock Socket Length (ft.)	Nominal Unit Side Shear q_{ss} (ksf)	Nominal Unit End Bearing q_{eb} (ksf)	Nominal Side Resistance R_{sr} (kips)	Nominal End Bearing Resistance R_{eb} (kips)	Factored Side Resistance ϕR_{sr} (kips)	Factored End Bearing Resistance ϕR_{eb} (kips)	Total Factored Axial Resistance ϕR_t (kips)	Total Factored Uplift Resistance ϕR_{tu} (kips)
0.0								
1.0	32.7	72	770	3181	423	1590	2014	308
2.0	32.7	72	1539	3181	847	1590	2437	616
3.0	32.7	72	2309	3181	1270	1590	2860	924
4.0	32.7	72	3078	3181	1693	1590	3284	1231
5.0	32.7	72	3848	3181	2116	1590	3707	1539
6.0	32.7	72	4618	3181	2540	1590	4130	1847
7.0	32.7	72	5387	3181	2963	1590	4553	2155
8.0	32.7	72	6157	3181	3386	1590	4977	2463
9.0	32.7	72	6926	3181	3810	1590	5400	2771
10.0	32.7	72	7696	3181	4233	1590	5823	3078
11.0	32.7	72	8466	3181	4656	1590	6247	3386
12.0	32.7	72	9235	3181	5079	1590	6670	3694
13.0	32.7	72	10005	3181	5503	1590	7093	4002
14.0	32.7	72	10774	3181	5926	1590	7516	4310
>>> 15.0	32.7	72	11544	3181	6349	1590	7940	4618
16.0	32.7	72	12314	3181	6772	1590	8363	4925
17.0	32.7	72	13083	3181	7196	1590	8786	5233
18.0	32.7	72	13853	3181	7619	1590	9209	5541
19.0	32.7	72	14622	3181	8042	1590	9633	5849
20.0	32.7	72	15392	3181	8466	1590	10056	6157
AASHTO Table 10.5.5.2.4-1				Resistance Factor, ϕ	0.55	0.50		0.40
AASHTO 10.5.5.2.4: *When applying this table to a single shaft supporting a bridge pier, reduce the factored resistance by another 20%.								
>>> = Min. Socket Length							D (ft.) =	7.5

Load and Resistance Factor Design (LRFD)

DRILLED SHAFT AXIAL RESISTANCE TABLE

S-002-2021: Jefferson Co., Item# 5-804.00, I-264 over I-71

S-002-2021 05-0804.00 Kentucky Transportation Cabinet

ID	Latitude	Longitude	Hole	Station	Offset	Elevation(ft)	Comments
1	38.2885026	-85.6457981	B-1011	45+91.7	59	570.53	
2	38.2883533	-85.6460164	B-1012	45+94.5	-24	540.35	
3	38.2887187	-85.6464139	B-1013	47+69.6	-17	519.37	
4	38.288882	-85.6462938	B-1014	47+89.7	48.8	569.72	